

## SPECIFICATION

### TITLE OF THE INVENTION

Wavelength filter and wavelength monitor

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### TECHNICAL FIELD

The present invention relates to a wavelength filter for selecting a wavelength of a laser light output from a semiconductor laser module and a wavelength monitor for measuring an emission wavelength of a 10 laser light using the wavelength filter, that are used for a wavelength division multiplexing (WDM) transmission.

### BACKGROUND ART

For a wavelength monitor, there is a scheme in which an etalon filter is used as the wavelength monitor that detects an emission wavelength of a semiconductor laser. The etalon filter includes two flat reflecting surfaces, and with the flat reflecting surfaces, the etalon filter resonate light between the reflecting surfaces to transmit or reflect a specific wavelength. A solid etalon filter, in particular, is possible to be 20 structured with a single part because such as structure can be obtained using an optically transparent material that a reflecting film is formed on an input/output facet. In a following description, a wavelength monitor using the solid etalon filter is explained.

The etalon filter has a characteristic in which a transmissivity 25 varies depending on a wavelength. Therefore, it is possible to obtain a

wavelength discriminating signal that is intensity information converted from wavelength information by making a laser light pass through the etalon filter. In this case, it is an important condition for monitoring the wavelength with high precision that a characteristic for discriminating 5 the wavelength does not vary as a condition of an external environment, such as ambient temperature, changes. However, temperature dependence of the characteristic for discriminating the wavelength is dependent on a characteristic of a material of the etalon filter, and is expressed as

$$10 \quad \frac{d\lambda}{dT} = \frac{dn/dT + \alpha}{n} \cdot \lambda \quad (1)$$

where  $dn/dT$  is temperature-dependent variation of a refractive index, and  $\alpha$  is a linear expansion coefficient.

Materials generally used for the etalon includes glass. However, with glass available at present, a numerator of on right side of 15 the Eq. (1) is not zero. Therefore, in glass as a etalon material, there is a problem in which a wavelength discriminating characteristic varies according to a temperature change.

Many studies on development of an etalon filter that has no temperature dependence have been conducted up to now. In 20 conventional technologies for realizing the etalon filter that has no temperature dependence, there is a method in which a material is used that a linear expansion coefficient compensates a ratio of change of the refractive index with respect to temperature (see, for example, Patent Literature 1). Fig. 1 is a schematic for illustrating an axis structure and

a direction of an incident axis of the etalon filter described in the Patent Literature 1. In an etalon filter 100, for example, a birefringent crystal LiSAF (LiSrAlF<sub>6</sub>) is used as the material of which a linear expansion coefficient compensates for a ratio of change of the refractive index 5 with respect to the temperature. A reflecting mirror mechanism is adopted on a laser-light incident plane and an output plane of the etalon filter 100. Because the LiSAF crystal is a single-axis birefringent crystal, the LiSAF crystal has an optical anisotropy, and includes an optical axis (hereinafter, "c-axis") and two axes (hereinafter, "a-axis" 10 and "b-axis") having a refractive index and a linear expansion coefficient different from those of the c-axis. Therefore, when a laser incident angle with respect to the c-axis is  $\theta$ , an optical length change of the etalon filter 100 due to a temperature change is expressed as

$$\frac{dnL}{d\Delta T} = \frac{d}{d\Delta T} \sqrt{[(n_c + dn_c \Delta T) \cos(\theta)]^2 + [(n_{ab} + dn_{ab} \Delta T) \sin(\theta)]^2} \quad (2)$$

$$\sqrt{[(1 + dn_c \Delta T) \cos(\theta)]^2 + [(1 + dn_{ab} \Delta T) \sin(\theta)]^2}$$

15 where nL is the optical length, n<sub>c</sub> is a refractive index experienced by a laser light having a polarizing plane that is in parallel with a plane made by the c-axis and a direction of the optical axis, n<sub>ab</sub> is a refractive index experienced by a laser light having a polarizing plane that is the same as a plane perpendicular to n<sub>c</sub>,  $\Delta T$  is an amount of the temperature change, dn<sub>c</sub> is a shift amount of the refractive index n<sub>c</sub> per unit temperature change, and dn<sub>ab</sub> is a shift amount of the refractive index n<sub>ab</sub> per unit temperature change.

The optical length nL with which zero is obtained in Eq. (2) by

changing the laser-light incident angle  $\theta$  with respect to the c-axis is the condition for achieving no temperature dependence, i.e., the condition for obtaining a wavelength discriminating characteristic that does not change with a temperature change. In this example of the

5 conventional technology, setting  $\theta=36.55^\circ$  using LiSAF for the etalon material satisfies a condition with which the etalon filter 100 has no temperature dependence.

#### Patent Literature 1

US Patent No. 6,452,725

10 However, a fixing of the etalon filter 100 causes a change of the optical characteristic of the etalon filter 100 when the etalon filter 100 is installed in a wavelength monitor or in a semiconductor laser module including the wavelength monitor. As a result, parameters of the etalon filter 100 are deviated from the condition for achieving no temperature dependence, and when the etalon filter 100 is used for the wavelength monitor, the wavelength discriminating characteristic changes with a temperature change.

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Furthermore, a change of the temperature characteristic by the laser-light incident angle  $\theta$  with respect to the c-axis greatly shifts at a vicinity of the angle  $\theta$  with which the condition for achieving no temperature dependence is satisfied, the condition for achieving no temperature dependence is easily deviated by a subtle change of an angle of an incident laser light.

In view of the above, and it is an object of the present invention  
25 to provide a wavelength filter that satisfies the condition for achieving

no temperature dependence even when the wavelength filter is fixed at a holder and a wavelength monitor using the wavelength filter.

#### DISCLOSURE OF THE INVENTION

5       A wavelength filter according to the present invention includes a solid material that is optically transparent; a pair of flat planes formed on the sold material substantially in parallel with each other; and a supporting member that supports the solid material on a plane of the solid material other than the pair of flat planes with an adhesive agent,

10      the supporting member having a rigidity stronger than that of the solid material. The light is resonated between the pair of flat planes, the wavelength filter selects a wavelength that is determined by an optical length between the pair of flat planes, and the solid material is a birefringent material of which an optical axis makes a predetermined

15      angle with respect to a normal to the pair of flat planes.

         A wavelength monitoring apparatus according to the present invention includes a wavelength filter that includes a solid material that transmits the laser light, and a pair of flat planes formed on the sold material substantially in parallel with each other, the wavelength filter

20      selecting a wavelength determined by an optical length between the pair of flat planes in a cycle by resonating the laser light between the pair of flat planes; a wavelength detecting unit that measures an emission wavelength of the laser light based on a transmission light from the wavelength filter; and a supporting member that supports the

25      wavelength detecting unit and the wavelength filter on a plane of the

wavelength filter other than the pair of flat planes with an adhesive agent, the supporting member having a rigidity stronger than that of the solid material. The wavelength monitoring apparatus detects a wavelength of a laser light output from a semiconductor laser, and the 5 solid material is a birefringent material of which an optical axis makes a predetermined angle with respect to a normal to the pair of flat planes.

#### BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a schematic of a configuration of a conventional optical  
10 filter; Fig. 2 is a schematic of a wavelength filter according to a first embodiment of the present invention; Fig. 3 is a graph for illustrating a relation between an angle  $\phi_c$  between an optical axis and c-axis and a temperature characteristic of a wavelength characteristic in a single piece of filter according to the first embodiment; Fig. 4 is a graph for  
15 illustrating a temperature characteristic of a single piece of etalon filter according to the first embodiment; Fig. 5 is a graph for illustrating a temperature characteristic of the single piece of etalon filter according to the first embodiment when the etalon filter is fixed in a holder; Fig. 6 is an enlarged graph of temperature dependence of the angle  $\phi_c$   
20 between the optical axis and the c-axis of the filter according to the first embodiment and the wavelength characteristic; Fig. 7 is a schematic of a configuration of a semiconductor laser module that includes a wavelength monitor according to a second embodiment of the present invention; Fig. 8 is a graph of temperature dependence of an angle  $\phi_c$   
25 between the optical axis and the c-axis and wavelength characteristics

of a single piece of etalon filter according to the second embodiment; and Fig. 9 is a graph that indicates a wavelength-monitor signal characteristic of the semiconductor laser module according to the second embodiment.

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## BEST MODE FOR CARRYING OUT THE INVENTION

Exemplary embodiments of a wavelength filter and a wavelength monitor according to the present invention will be explained in detail below with reference to the accompanying drawings.

### 10 First Embodiment

Fig. 2 is a schematic of a wavelength filter according to a first embodiment of the present invention. As shown in Fig. 2, a wavelength filter has a structure in which an etalon filter 1 is supported on a holder 2 by an adhesive agent 3. In the fist embodiment, a traveling direction (direction of light axis) of a laser light is determined as a direction of z-axis in space coordinates, an upward direction in a space is determined as a direction of y-axis, and a downward direction in the space is determined as a direction of x-axis.

The etalon filter 1 includes reflecting films 5, 6 on an incident plane and an output plane of the laser light, and is formed with an optically-uniaxial birefringent crystal (such as,  $\alpha$ -BBO ( $\text{BaB}_2\text{O}_4$ ) crystal,  $\text{LiIO}_3$  crystal,  $\text{CaCO}_3$  crystal, and  $\beta$ -BBO crystal). The optically-uniaxial birefringent crystal used as the etalon filter 1 is cut in such a manner that c-axis of the optically-uniaxial birefringent crystal is arranged to make a predetermined angle  $\phi_c$  with respect to an optical axis of the

laser light (z-axis), and a cutout plane of the optically-uniaxial birefringent crystal is arranged in parallel with an xy-plane that is perpendicular to the optical axis (z-axis).

The holder 2 is a substrate that supports the etalon filter 1.

5      The holder 2 is bigger than the etalon filter 1, and is formed with a material having rigidity higher than that of the etalon filter 1. As for a material for the holder 2, for example, a CuW substrate can be used. The holder 2 supports a plane of the etalon filter 1 other than the plane on which the reflecting films 5, 6 are formed (i.e., as long as the optical 10 path of the etalon filter 1 is not blocked, any plane can be used).

The adhesive agent 3 fixes the holder 2 and the etalon filter 1 by bonding the holder 2 and the etalon filter 1. As for a material for the adhesive agent 3, for example, an ecobond SOLDER56C (trade name) that is a conductive adhesive-agent manufactured by EMERSON, Ltd. 15 can be used.

A transmission characteristic of the laser light transmitted through the etalon filter 1 with respect to the wavelength is kept constant regardless of changes of temperature of the etalon filter 1, the adhesive agent 3, and the holder 2.

20      Following is an explanation of a condition for no temperature dependence of the etalon filter 1 that is fixed on the holder 2 by the adhesive agent 3. A laser light A4 incident on an incident plane 5 of the etalon filter 1 that is fixed on the holder 2 shown in Fig. 2 has a p-polarized light in parallel with the x-axis. In the etalon filter 1, the 25 c-axis of the optically-uniaxial birefringent crystal in on a yz-plane, the

optical axis is in parallel with the z-axis, and the c-axis makes a predetermined angle  $\phi_c$  (hereinafter, "optical axis angle") with respect to the optical axis. An ordinary light is perpendicular to a plane made by the c-axis and the optical axis with a same oscillation plane as a plane 5 that is in parallel with the optical axis. Therefore, in this case, the laser light A4 propagates through the etalon filter 1 as the ordinary light.

Before explaining a temperature characteristic of the etalon filter 1 in a state in which the etalon filter 1 is fixed on the holder 2, a temperature characteristic of a single piece of the etalon filter 1 will be 10 explained. The temperature characteristic of refractive index experienced by the laser light that transmits through the etalon filter 1 is expressed as  $dn_o/dT$  using ordinary-light-axis refractive index  $n_o$ . A linear expansion coefficient  $\alpha(\phi_c)$  is expressed as

$$\alpha(\phi_c) = \alpha_c \cos^2 \phi_c + \alpha_a \sin^2 \phi_c \quad (3)$$

15 where  $\alpha_c$  is a linear expansion coefficient in a direction parallel to the c-axis, and  $\alpha_a$  is a linear expansion coefficient in a direction perpendicular to the c-axis.

A temperature dependence of a wavelength characteristic with respect to the ordinary light can be expressed as

$$20 \quad \frac{d\lambda}{dT} = \frac{dn_o/dT + \alpha(\phi_c)}{n_o} \quad \lambda_0 \quad (4)$$

using  $dn_o/dT$  and  $\alpha(\phi_c)$ .

When a laser light 4B output from the etalon filter 1 has an s-polarized light in parallel with the y-axis, it is the case that the laser light 4A propagates through the etalon filter 1 as an extraordinary light.

In this case, the refractive index experienced by the laser light is expressed as a function of the angle  $\phi_c$  between the c-axis and the optical axis, and the temperature dependence of the wavelength characteristic is expressed as

$$5 \quad \frac{d\lambda}{dT} = \frac{dn(\phi_c)/dT + \alpha(\phi_c) n(\phi_c)}{n(\phi_c)} \lambda_0 \quad (5)$$

where  $dn(\phi_c)/dT$  is a temperature coefficient of the refractive index  $n(\phi_c)$  experienced by the extraordinary light, expressed as

$$\frac{dn(\phi_c)}{dT} = \frac{d}{dT} n_0 \sqrt{\frac{1 + \tan^2 \phi_c}{1 + (n_0/n_e)^2 \tan^2 \phi_c}} \quad (6)$$

Fig. 3 is a graph for illustrating a relation between the angle  $\phi_c$   
 10 and the temperature characteristic of the wavelength characteristic in  
 the extraordinary light and the ordinary light calculated using Eq. (4)  
 and Eq. (5) when CaCo<sub>3</sub> crystal is used as the material for the etalon  
 filter 1. The physical constants of the CaCo<sub>3</sub> used in the calculation  
 are as follows: the extraordinary-light refractive index  $n_e$  is 1.4771, the  
 15 ordinary-light refractive index  $n_o$  is 1.6337, the temperature coefficient  
 of refractive index in a direction of extraordinary light axis  $dn_e/dT$  is  
 $1.19 \times 10^{-5}/K$ , the temperature coefficient of refractive index in a  
 direction of ordinary light axis  $dn_o/dT$  is  $2.10 \times 10^{-6}/K$ , the linear  
 expansion coefficient  $\alpha_a$  is  $-5.70 \times 10^{-6}/K$ , and the linear expansion  
 20 coefficient  $\alpha_c$  is  $2.44 \times 10^{-6}/K$ . From Fig. 3, it is found that the  
 temperature characteristic can be freely set from  $+4 \text{ pm}/^\circ\text{C}$  to  $+40$   
 $\text{pm}/^\circ\text{C}$  in a direction of the extraordinary light axis, and  $-7 \text{ pm}/^\circ\text{C}$  to  $+40$   
 $\text{pm}/^\circ\text{C}$  in a direction of the ordinary light axis, by changing the optical

axis angle  $\phi_c$ . For instance, the condition for no temperature dependence for  $\text{CaCO}_3$  crystal when using the ordinary light can be obtained as a point at which the temperature characteristic of the ordinary light becomes zero, i.e., a vicinity of the optical axis angle of  
 5       $63^\circ$ .

Following is an explanation of the temperature characteristic of the etalon filter 1, a single piece of the optically-uniaxial birefringent material, with respect to the optical axis angle  $\phi_c$  in a state in which the etalon filter 1 is fixed on the holder 2 by the adhesive agent 3. The  
 10     thickness of the adhesive agent 3 is thin enough so that a thermal characteristic of the adhesive agent 3 can be ignored. A linear expansion coefficient of the holder 2 is defined as  $\alpha_2$ . Since the holder 2 has a rigidity stronger than that of the etalon filter 1, an effective linear expansion coefficient of the etalon filter  $\alpha'$  can be expressed as  
 15      $\alpha' = \alpha_2 - \alpha(\phi_c)$

Besides, to incorporate a refractive index change due to a strain (photo-elastic effect), a photo-elastic constant in a direction of the z-axis is set as  $P_{zo}$ , and a photo-elastic constant in a direction of the x-axis is set as  $P_{xo}$ , when the ordinary light is incident (a photo-elastic constant in a direction of the z-axis is set as  $P_{ze}$ , and a photo-elastic constant in a direction of the x-axis is set as  $P_{xe}$ , when the extraordinary light is incident). Since an amount of the strain due to a thermal expansion is expressed by a difference of the linear expansion coefficients of the etalon filter 1 and the holder 2, a change of refractive  
 20     index due to the strain in a direction of the z-axis can be expressed as  
 25

in the case of the ordinary light,

$$\Delta n_{zo} = -\frac{1}{2} n_o^3 P_{zo} (\alpha_2 - \alpha(\phi_c)) \quad (8)$$

and in the case of the extraordinary light,

$$\Delta n_{xe} = -\frac{1}{2} n(\phi_c)^3 P_{xe} (\alpha_2 - \alpha(\phi_c)) \quad (8')$$

5 A change of refractive index due to the strain in a direction of the x-axis can be expressed as

in the case of the ordinary light

$$\Delta n_{xo} = -\frac{1}{2} n_o^3 P_{xo} (\alpha_2 - \alpha_a) \quad (9)$$

and in the case of the extraordinary light

$$10 \quad \Delta n_{xe} = -\frac{1}{2} n(\phi_c)^3 P_{xe} (\alpha_2 - \alpha_a) \quad (9')$$

Assuming that the strain in a direction of the y-axis is small enough to be ignored, it can be considered that  $\Delta n_{xo}$  and  $\Delta n_{zo}$  are added to the temperature coefficient of the refractive index in the case of the ordinary light. Then, the temperature coefficient of the refractive index in a direction of the ordinary light  $dn'/dT$  can be expressed as

$$\begin{aligned} \frac{dn'}{dT} &= \frac{dn_o}{dT} + \Delta n_{zo} + \Delta n_{xo} \\ &= \frac{dn_o}{dT} - \frac{1}{2} n_o^3 P_{zo} (\alpha_2 - \alpha(\phi_c)) - \frac{1}{2} n_o^3 P_{xo} (\alpha_2 - \alpha_a) \end{aligned} \quad (10)$$

Similarly, the temperature coefficient of the refractive index in a direction of the extraordinary light can be expressed as

$$\begin{aligned}\frac{dn'}{dT} &= \frac{dn(\phi_c)}{dT} + \Delta n_{ze} + \Delta n_{xe} \\ &= \frac{dn(\phi_c)}{dT} - \frac{1}{2}n(\phi_c)^3 P_{ze} (\alpha_2 - \alpha(\phi_c)) - \frac{1}{2}n(\phi_c)^3 P_{xe} (\alpha_2 - \alpha_a)\end{aligned}\quad (11)$$

From these equations, the temperature dependence of the wavelength characteristic when the etalon filter 1 is fixed on the holder 2 can be expressed as

5 in the case of the ordinary light

$$\frac{d\lambda}{dT} = \frac{dn'/dT + \alpha' n_o}{n_o} \lambda_0 \quad (12)$$

and in the case of the extraordinary light

$$\frac{d\lambda}{dT} = \frac{dn'/dT + \alpha' n(\phi_c)}{n(\phi_c)} \lambda_0 \quad (13)$$

From Eqs. (12) and (13), because the temperature dependences  
 10 of the wavelength characteristic in the both cases are functions of the optical axis angle  $\phi_c$ , it is possible to satisfy the condition for no temperature dependence by selecting the optical axis angle  $\phi_c$  that makes the numerator of the right side zero. Furthermore, because the temperature characteristic of the single piece of the etalon filter 1 can  
 15 be freely changed within the range shown in Fig. 3 by adjusting the optical axis angle  $\phi_c$ , even when an optional adhesive agent 3 and an optional holder 2 are used, it is possible to fix the etalon filter 1 under the condition for no temperature dependence or a condition close to the condition for no temperature dependence. Although, in the first  
 20 embodiment, only a bottom plane of the etalon filter 1 is fixed on the holder 2, any plane of the etalon filter can be fixed as long as the

optical path is not blocked. For instance, using a holder having a configuration in which all side planes with respect to the optical axis are covered can obtain the same effect.

The above explanation is for a case of obtaining the condition  
5 for no temperature dependence of the etalon filter 1 that is fixed on the holder 2 using Eqs. (12) and (13). Following is an explanation for a method of obtaining the condition for no temperature dependence when the etalon filter 1 is fixed on the holder 2 without using the Eqs. (12) and (13).

10 Fig. 4 is a graph of the wavelength characteristic of the single piece of etalon filter (in a state in which the etalon filter is not fixed on the holder) when the temperature is changed; and Fig. 5 is a graph of the wavelength characteristic in a state in which the same etalon filter is fixed on the holder. In the experiment for obtaining the wavelength  
15 characteristics shown in these figures, a  $\text{CaCO}_3$  crystal having an optical axis angle  $\phi_c=65.7^\circ$  and a thickness (length of the crystal in a direction of the z-axis) of 3.6 mm is used for the material for the etalon filter 1, and the conductive adhesive-agent manufactured by EMERSON, Ltd., ecobond SOLDER56C (trade name), is used for the material for  
20 the adhesive agent 3. From these figures, the temperature characteristics are obtained as  $0.23 \text{ pm}/^\circ\text{C}$  and  $0.45 \text{ pm}/^\circ\text{C}$ , respectively.

Fig. 6 is an enlarged graph of a vicinity of the optical axis angle  
25  $\phi_c=66.0^\circ$  in the graph shown in Fig. 3, with a plotting of data of the temperature characteristic obtained from Fig. 4 and Fig. 5. From Fig.

6, it is found that the optical axis angle  $\phi_c$  that satisfies the condition for no temperature dependence is deviated due to a fixing of the etalon filter 1 on the holder 2. In other words, by shifting the optical axis angle from the optical axis angle  $\phi_c=66.0^\circ$  that satisfies the condition for 5 no temperature dependence obtained for the single piece of the etalon filter 1 to the optical axis angle  $\phi_{c1}=66.3^\circ$  that satisfies the condition for no temperature dependence for the etalon filter 1 fixed on the holder 2, the etalon filter 1 fixed on the holder 2, having a structure with a wavelength characteristic that does not change with a temperature 10 change, can be obtained.

Although, an aluminum substrate is used for the holder 2 and the conductive adhesive agent is used for the adhesive agent 3 in this experiment, even when the holder 2 and the adhesive agent 3 made of other materials are used, it is possible to obtain the optical axis angle  $\phi_c$  15 that satisfies the condition for no temperature dependence by measuring the temperature dependence of the wavelength characteristic due to a fixing of the etalon filter 1 on the holder 2.

Furthermore, although the  $\text{CaCO}_3$  crystal is used for the material for the etalon filter 1 in the first embodiment, other optically-uniaxial 20 birefringent materials, such as  $\alpha$ -BBO crystal,  $\beta$ -BBO crystal, and  $\text{LiIO}_3$  crystal, can also be used. Even in the case in which other optically-uniaxial birefringent materials are used, it is possible to obtain a condition for no temperature dependence with respect to the optical axis angle  $\phi_c$ , as shown in Fig. 3, and it is possible to obtain the optical 25 axis angle  $\phi_c$  that satisfies the condition for no temperature dependence

for the etalon filter 1 fixed on the holder 2 using Eqs. (12) and (13).

Moreover, although the etalon 1 is fixed on the holder 2 using the adhesive agent 3 in the first embodiment, other fixing methods can also be used, such as a soldering and a YAG welding. Even in the 5 case in which other fixing methods are used, it is possible to achieve the no temperature dependence of the etalon filter 1 fixed on the holder 2, by adjusting the optical axis angle  $\phi_c$  of the etalon filter 1 after fixing the etalon filter 1 on the holder 2.

As explained above, according to the first embodiment, a 10 structure, with which a condition for no temperature dependence when the etalon filter 1 is fixed on the holder 2 is satisfied, can be obtained by considering an effective linear expansion coefficient and a refractive index change due to a photo-elastic effect by a strain caused by a difference of the rigidity between the etalon filter 1 and the holder 2 in 15 addition to a change of temperature characteristic with respect to the optical axis angle  $\phi_c$  of a single piece of the etalon filter 1. In other words, even if a material for the holder 2 and a material for the adhesive agent 3 having optional linear expansion coefficients are used 20 for fixing the etalon filter 1, by obtaining the optical axis angle  $\phi_c$  that satisfies the condition for no temperature dependence from the temperature characteristic of the etalon filter 1 fixed by each of the 25 combinations of the materials, it is possible to obtain the condition for no temperature dependence for the etalon filter 1 fixed by the combination of the materials. In this manner, even with the etalon filter 1 having a temperature dependence in a state of a single piece of

crystal, it is possible to achieve a structure that satisfies the condition for no temperature dependence in a state in which the etalon filter 1 is fixed on the holder 2. Therefore, the wavelength characteristic of the etalon filter 1 obtained from this structure is not affected by the  
5 temperature change.

According to the first embodiment, the laser light from the semiconductor laser is set to a p-polarized light, and the laser light is incident on the etalon filter 1 as an ordinary light. However, the laser light from the semiconductor laser can be set to an s-polarized light,  
10 and the laser light can be incident on the etalon filter 1 as an extraordinary light. In this case, the same effect can be achieved by using the optical axis angle  $\phi_c$  that satisfies Eq. (13), i.e., by using the optical axis angle  $\phi_c$  that satisfies the condition for no temperature dependence in a state in which the etalon filter 1 is fixed on the holder  
15 2.

#### Second Embodiment

According to a second embodiment of the present invention, a semiconductor laser module that includes a wavelength monitor equipped with an etalon filter according to the first embodiment, which  
20 is fixed on a holder, having no temperature dependence is explained.

Fig. 7 is a schematic diagram of a semiconductor laser module equipped with a wavelength monitor according to the second embodiment. According to the second embodiment, a traveling direction of a laser light (a direction of the optical axis) is determined as  
25 z-axis in a space coordinates, an upward direction in a space (a

protruding direction perpendicular to a surface of the paper in fig. 3) is determined as a direction of y-axis, a direction perpendicular to the z-axis and the y-axis is determined as a direction of x-axis, and a position at which a semiconductor laser 10 is installed is determined as 5 an origin of the z-axis.

The semiconductor laser module has a structure in which a wavelength monitor 20 equipped with the etalon filter 1 fixed on the holder according to the first embodiment, and a Peltier cooler 16 connected to a bottom surface of the wavelength monitor 20 are 10 assembled in a module package 17 that shields against the outside air.

The wavelength monitor 20 includes the etalon filter 1 that transmits a specific wavelength only, the semiconductor laser 10 that outputs a laser light, a first lens 11 that is arranged in front of the semiconductor laser 10 (a positive direction of the z-axis) and adjusts a 15 beam diameter of the laser light output from the semiconductor laser 10 (hereinafter, "an optical signal"), and a second lens 18 that is arranged behind the semiconductor laser 10 (a negative direction of the z-axis) and adjusts the laser light output from the semiconductor laser 10.

The etalon filter 1 is an etalon made of the optically-uniaxial 20 birefringent crystal according to the first embodiment, such as  $\alpha$ -BBO crystal,  $\text{CaCO}_3$  crystal,  $\text{LiIO}_3$  crystal, and  $\beta$ -BBO crystal. A reflecting film is formed on an input facet and an output facet of the etalon filter 1 for the laser light, and the etalon filter 1 is installed in such a manner that the input facet and the output facet is perpendicular to the optical 25 axis. The c-axis of the etalon filter 1 is in the yz-plane, as shown in

Fig. 2, making a predetermined angle  $\phi_c$  with respect to the optical axis.

The semiconductor laser 10 is a laser that can tune a wavelength of the laser light by adjusting an injection current or a temperature, such as a distributed feedback (DFB) laser having a grating in an active layer, a wavelength-tunable laser that can tune the wavelength of the laser light by adjusting the injection current or the temperature (such as a distributed bragg reflector (DBR) laser and a vertical cavity surface emitting laser (VCSEL)), and an EA modulator-integrated laser diode (EA-LD) in which an electro-absorption device and a laser diode are integrated. The input facet and the output facet of the etalon filter 1 for the optical signal are substantially perpendicular to the optical axis.

The wavelength monitor 20 further includes a first light sensitive element 12 that converts the optical signal passed through the first lens 11 into an electrical signal, and a second light sensitive element 13 that converts the optical signal passed through the first lens 11 and the etalon filter 1 into an electrical signal.

The etalon filter 1, the first lens 11, the first light sensitive element 12, the second light sensitive element 13, and the second lens 18 are fixed on a carrier 14. The carrier 14 is bigger enough than the etalon filter 1, made of a material having a rigidity stronger than that of the etalon filter 1, and equivalent to the holder 2 according to the first embodiment.

The wavelength monitor 20 further includes a thermistor 15 that detects a temperature signal. The thermistor 15 is directly fixed on the

carrier 14.

The Peltier cooler 16 is connected on a bottom surface of the carrier 14. By driving the Peltier cooler 16 using the temperature signal from the thermistor 15, it is possible to carry out a temperature control of the entire carrier 14. With this mechanism, it is possible to tune the wavelength of the semiconductor laser 10.

On a wall of the module package 17, a window 19 is arranged to emit the laser light that is output from the semiconductor laser 10 in the wavelength monitor 20, and passed through the second lens 18 to outside.

Following is an explanation for an operation of the semiconductor laser module having the above structure. A laser light having a plane of polarization oscillating in the direction of the x-axis is output from the semiconductor laser 10 in both positive and negative direction of the z-axis. The laser light output in the positive direction of the z-axis (optical signal) is collimated by the first lens 11. The axis passing through the semiconductor laser 10 and a center of the first lens 11 becomes the optical axis. On the other hand, the laser light output in the negative direction of the z-axis is collimated by the second lens 19, and passes through the window 19 to be output to the outside of the module package 17 as an optical signal. From this point on, a case in which the optical signal output on a side of the first lens 11 is explained.

A half of a cross section of a beam of the laser light (optical signal) passed through the first lens 11 (an area of the optical signal on

a side of the direction of the x-axis from the optical axis shown in Fig. 7) is directly input to the first light sensitive element 12. The first light sensitive element 12 is arranged with an input facet slant against the optical axis between the first lens 11 and the etalon filter 1 along the 5 z-axis in such a manner that the half of the cross section of the beam of the optical signal is input to the input facet. The first light sensitive element 12 receives the optical signal from the semiconductor laser 10, which does not pass through the etalon filter 1, detects an intensity of the optical signal, and outputs a power monitor signal. Because the 10 power monitor signal is proportional to an output intensity of the semiconductor laser 10, it is possible to stabilize the laser light output from the semiconductor laser 10 at an optional output intensity by controlling the injection current to the semiconductor laser 10 using the power monitor signal. Furthermore, as shown in the figure, the first 15 light sensitive element 12 is arranged closer to the semiconductor laser 10 than the etalon filter 1, a transmission light having a predetermined wavelength characteristic output from the etalon filter 1 is not input to the input facet of the first light sensitive element 12.

The second light sensitive element 13 is arranged at a 20 subsequent stage of the etalon filter 1 (the positive direction of the z-axis) with an input facet slant against the optical axis. The second light sensitive element 13 receives a component of the laser light passed through the etalon filter 1 from among the component of the rest of the cross section of the beam of the optical signal that is not received 25 by the first light sensitive element 12. The second light sensitive

element 13 detects an intensity of the laser light received, and outputs a wavelength monitor signal. The wavelength monitor signal indicates a wavelength discriminating characteristic based on the wavelength characteristic of the etalon filter 1. Therefore, it is possible to stabilize 5 the wavelength of the laser light output from the semiconductor laser 10 by controlling the injection current to the semiconductor laser 10 or the temperature, using an error signal between a wavelength obtained from the wavelength monitor signal and a target wavelength for stabilization.

Furthermore, by normalizing the wavelength monitor signal with the 10 power monitor signal output from the first light sensitive element 12, a normalized wavelength monitor signal that does not depend on a change of the intensity of the laser light from the semiconductor laser 15 can be obtained. By using the normalized wavelength monitor signal, it is possible to realize a wavelength stabilization of the laser light output from the semiconductor laser 10 with even higher precision.

Fig. 8 is a graph of temperature dependence of the wavelength characteristic with respect to the optical axis angle  $\phi_c$  for the ordinary light and the extraordinary light when a single piece of the  $\alpha$ -BBO crystal is used as the etalon filter 1. The physical constants used in 20 the calculation are as follows: the extraordinary-light refractive index  $n_e$  is 1.53003, the ordinary-light refractive index  $n_o$  is 1.6502, the temperature coefficient of refractive index in a direction of extraordinary light axis  $dn_e/dT$  is  $1.60 \times 10^{-5}/K$ , the temperature coefficient of refractive index in a direction of ordinary light axis  $dn_o/dT$  is  $-9.15 \times 10^{-6}/K$ , the 25 linear expansion coefficient  $\alpha_a$  is  $7.17 \times 10^{-6}/K$ , and the linear expansion

coefficient  $\alpha_c$  is  $1.92 \times 10^{-6}/K$ .

From Fig. 8, it is found that the temperature characteristic can be freely set from  $+9.5 \text{ pm}^{\circ}\text{C}$  to  $+21 \text{ pm}^{\circ}\text{C}$  in a direction of the extraordinary light axis, and  $+2.5 \text{ pm}^{\circ}\text{C}$  to  $+21 \text{ pm}^{\circ}\text{C}$  in a direction of  
5 the ordinary light axis, by changing the optical axis angle  $\phi_c$  of the  $\alpha$ -BBO crystal on the  $yz$ -plane from  $0^{\circ}$  to  $90^{\circ}$ . Following explanation is for a case in which the optical axis angle  $\phi_c$  of the etalon filter 1 is set to  
90°.

According to the second embodiment, the laser light (optical  
10 signal) incident on the etalon filter 1 propagates through the etalon filter 1 as in the case of the first embodiment, and under the above conditions, a single piece of the etalon filter 1 has a temperature characteristic of as low as  $2.5 \text{ pm}^{\circ}\text{C}$ . Furthermore, because a temperature dependence due to a change of the optical axis angle  $\phi_c$  is  
15 small at the optical axis angle  $\phi_c (=90^{\circ})$ , a change of the temperature characteristic due to a deviation of an angle of the laser light is small. Moreover, because the optical axis angle  $\phi_c$  of the etalon filter 1 is set to a right angle, and the input facet is also arranged at a right angle, a change of the wavelength characteristic with respect to a deviation of  
20 the optical axis is suppressed.

In addition, by setting a thickness of the etalon filter 1 (a length of the crystal in the direction of the  $z$ -axis) to approximately 3.5 mm, and setting a free spectral range (FSR) that is a cycle range of the wavelength characteristic to 25 GHz, it is possible to comply to 25 GHz  
25 range of International Telecommunication Union Telecommunication

Standardization Sector (ITU-T) grid.

Because, the etalon filter 1 is fixed on the carrier 14 by an adhesive agent (for example, a conductive adhesive-agent manufactured by EMERSON, Ltd., ecobond SOLDER56C (trade name)),

5 it is near the condition for no temperature dependence in this state, considering an effective linear expansion coefficient and a refractive index change due to a photo-elastic effect by a strain caused by a difference of the rigidity between the etalon filter 1 and the carrier 14, a explained in the first embodiment.

10 In a state in which a temperature of parts on the carrier 14 is controlled to a predetermined temperature by the thermistor 15 and the Peltier cooler 16, even if the temperature of the outside of the module package 17 is changed, there is ideally no change of the temperature on the carrier 14 in the module package 17 from a property of the

15 structure, although the temperature of the module package 17 is changed according to a temperature change of the outside. However, in practice, there is an extremely small amount of temperature change in each of the parts because there is a thermal resistance between the thermistor 15 and each of the parts.

20 With the structure of the wavelength monitor 20 according to the second embodiment, when the temperature of the outside air is changed from  $-20^{\circ}\text{C}$  to  $+70^{\circ}\text{C}$ , a temperature change of  $2^{\circ}\text{C}$  occurs on the etalon filter 1. For this reason, if the etalon filter 1 has a temperature dependence, the wavelength characteristic changes, and

25 as a result, the wavelength monitor signal cannot indicate a correct

value.

Fig. 9 is a graph of wavelength-monitor signal when the temperature of the outside air is set to  $-20^{\circ}\text{C}$ ,  $+25^{\circ}\text{C}$ , and  $+70^{\circ}\text{C}$ . The etalon filter 1 fixed on the carrier 14 shows a temperature dependence of  $2.5 \text{ pm}/^{\circ}\text{C}$  as a single piece of crystal. However, as explained in the first embodiment, with the etalon filter 1 fixed on the carrier 14 at near the condition for no temperature dependence, it is possible to suppress a wavelength drift within  $\pm 1 \text{ pm}$  in the entire etalon filter 1 fixed on the carrier 14 (i.e., the entire wavelength monitor), even when the temperature of the etalon filter 1 itself is changed by about  $2^{\circ}\text{C}$  with a change of the temperature of the outside air from  $-20^{\circ}\text{C}$  to  $+70^{\circ}\text{C}$ .

As explained above, according to the second embodiment, since the wavelength monitor 20 is configured with the c-axis angle of the uniaxial birefringent crystal as a material for the etalon filter 1 adjusted in such a manner that the temperature dependence of the wavelength characteristic is eliminated in a state in which the etalon filter 1 according to the first embodiment is bonded on the carrier 14, the etalon filter 1 can satisfy the condition for no temperature dependence or near the condition for no temperature dependence. As a result, the wavelength monitor signal can eliminate a change due to the temperature of the etalon filter 1, making a signal of high precision depending only on a emission wavelength of the semiconductor laser 10.

Furthermore, since the optical axis angle  $\phi_c$  of the  $\alpha\text{-BBO}$  crystal of the etalon filter 1 is set to  $90^{\circ}$ , as clearly shown in Fig. 8, it is

possible to reduce a change of the temperature characteristic due to a change of the optical axis angle  $\phi_c$  near this point. Therefore, it is possible to suppress a change of the temperature characteristic due to a deviation of an angle of the laser light. In addition, a change of the 5 wavelength characteristic with respect to a deviation of the optical axis can also be suppressed.

Although, the etalon filter 1 is arranged in such a manner that the input facet and the output facet are perpendicular to the optical axis, according to the second embodiment, the etalon filter 1 can also be 10 arranged at an angle other than the right angle. In such a case, an optical axis propagating in the etalon filter 1 is slant against an incident optical axis because of the refractive index of the etalon filter 1. However, setting of the optical axis angle  $\phi_c$  in such a manner that the condition for no temperature dependence according to the first 15 embodiment is satisfied, considering the tilt, can solve the problem. When the etalon filter is arranged with the input facet slant against the optical axis, as explained above, a reflected light from the etalon filter 1 having the wavelength characteristic does not return to the semiconductor laser 10, and as a result, it is possible to obtain a more 20 stabilized laser oscillation. Furthermore, because a stray light to the first light sensitive element 12 and the second light sensitive element 13 via the first lens 11 and a facet of the semiconductor laser 10 is suppressed, the power monitor signal and the wavelength monitor signal are not affected by the reflected light, either.

25 In addition, because the input facets of the first light sensitive

element 12 and the second light sensitive element 13 are tilted against the optical axis, an extremely small amount of reflected light from the first light sensitive element 12 and the second light sensitive element 13 does not return to the first lens 11 and the semiconductor laser 10, an

5 etalon effect between each of the input facets of the first light sensitive element 12 and the second light sensitive element 13 and the first lens 11 or the semiconductor laser 10 can be suppressed. Therefore, it is possible to obtain more stabilized power monitor signal and wavelength monitor signal.

10 Besides the  $\alpha$ -BBO crystal, an optional uniaxial birefringent crystal can be used as long as the material satisfies the condition for no temperature dependence according to the first embodiment, such as a  $\text{CaCo}_3$  crystal,  $\text{LiIO}_3$  crystal, and  $\beta$ -BBO crystal. In such a case, because it is possible to adjust the temperature dependence of a single 15 piece of the optional crystal by changing the optical axis angle  $\phi_c$ , even if a member for fixing the crystal on an optional carrier 14 is used (for example, the adhesive agent 3), the condition for no temperature dependence can be satisfied.

According to the second embodiment, the laser light from the 20 semiconductor laser is set to a p-polarized light, and the laser light is incident on the etalon filter 1 as an ordinary light. However, the laser light from the semiconductor laser can be set to an s-polarized light, and the laser light can be incident on the etalon filter 1 as an extraordinary light. In this case, the same effect can be achieved by 25 using the optical axis angle  $\phi_c$  that satisfies Eq. (13), i.e., by using the

optical axis angle  $\phi_c$  that satisfies the condition for no temperature dependence in a state in which the etalon filter 1 is fixed on the holder 2.

As explained above, according to the present invention, it is 5 possible to obtain a structure, with which a condition for no temperature dependence for the etalon filter fixed on the holder is satisfied, can be obtained by considering an effective linear expansion coefficient and a refractive index change due to a photo-elastic effect by a strain caused by a difference of the rigidity between the etalon filter and the holder in 10 addition to a change of temperature characteristic with respect to the optical axis angle  $\phi_c$  of a single piece of the etalon filter.

#### INDUSTRIAL APPLICABILITY

The present invention is suitable for applying to a wavelength 15 monitor of a semiconductor laser, as a light source, used in a wavelength-division-multiplexing communication and dense-wavelength-division-multiplexing communication employing an optical fiber, and applying to a wavelength filter used in the wavelength monitor.